

# Removal of Heavy Metals from an Actual Small Scale Gold Mining Wastewater by Sorption onto Cocopeat

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KEYWORDS Adsorption Cocopeat Heavy metals SSGM Wastewater ABSTRACT Cocopeat, a by-product of coconut husk, was used as adsorbent material to remove mercury (Hg) and other heavy metals (As, Ba, Cd, Pb) from the wastewater gathered from the tailings collection tank of a ball mill facility at the small scale gold mining (SSGM) area in Camarines Norte province, Philippines. Batch sorption tests were carried out using actual wastewater samples with reduced suspended solids collected after 60 min of settling and without modifying the pH and other parameters to simulate the actual condition in the field. Batch tests of water samples with an initial pH of 7.30 and adsorbent dose of 1.0 g cocopeat/L were tested for Lagergren first-order, pseudo-second-order, intraparticle diffusion, and Freundlich models to evaluate kinetic parameters and adsorption isotherms. The removal efficiencies obtained for the heavy metals after the equilibrium time of 240 min were 97.14%, 94.74%, 10.00%, 66.67%, and 27.01% for Hg, As, Ba, Cd, and Pb, respectively. The pseudo-second order kinetics model represented well the adsorption process as demonstrated with its higher correlation coefficients among the models.

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# 1. INTRODUCTION

Mercury and other heavy metals are present in the effluent and tailings from the SSGM ball mill facilities where the small scale miners use an amalgamation process with Hg to separate gold from mined ores. In 2000, the estimated consumption of Hg in the Philippines ranged from 20,000 to 30,000 kg/yr (Israel and Asirot 2002), being used in various SSGM sites in the country, including in the small scale mining sites in Paracale, Camarines Norte, located 320 km south of Manila. In 2007, small scale miners in Camarines Norte use 10-25 g of Hg to recover 1 g of gold from the ores, which is higher than the world usage average of 1 g Hg to recover 1 g of gold (Perez et al. 2007). These amounts of Hg together with other heavy metals are being released to the water bodies untreated as the inadequately designed sedimentation tanks serve as the only method for wastewater treatment. This practice becomes the basis of opposition to the amalgamation method because it affects the environment and human health (Israel and Asirot 2002; Velasquez-Lopez et al. 2010).

Mercury, which is one of the most toxic heavy metals released in the environment (Ahalya et al. 2003; Oboh et al. 2009), if present in rivers and lakes, it may be eaten by fish and in turn consumed by the people living in the area. Its major effects on human health include neurological and renal disturbances and impairment of pulmonary functions (Ahalya et al. 2003). Therefore, it is necessary to prevent Hg and other heavy metals from reaching water bodies such as creeks, rivers, and the sea. Several methods, such as reverse osmosis, electrodialysis, ultrafiltration, ion-exchange, chemical precipitation, and phytoremediation, are commonly used to remove heavy metals from mine tailings and other types of wastewater (Ahalya et al. 2003). These techniques were found to have disadvantages like incomplete metal removal, high reagent and energy requirements, and the generation of toxic sludges and other waste sludges that require careful disposal, all of which reduce its cost-effectiveness (Ahalya et al. 2003). Sorption of heavy metals on conventional adsorbents such as activated carbon have been widely used in many applications and found to be effective. Activated carbon, which is produced by carbonizing organic materials, is the most widely used adsorbent for wastewater treatment (Abdel Salam et al. 2011). However, this sorbent remains one of the expensive materials being used in removing heavy metals from wastewater (Abdel Salam et al. 2011; Kazemipour et al. 2008).

Agricultural waste is one of the rich sources of adsorbent due to its abundant availability (Abdel Salam et al. 2011). In the Philippines, one of the promising adsorbents from agricultural wastes is cocopeat. This material is a by-product of coconut husks during coconut fiber separation. Cocopeat consists mainly of lignin, cellulose, hemicellulose, and some pectin and extractives (mainly fat, fatty acids, fatty alcohols, phenols, terpenes, steroids, resin acids, rosin, and waxes) that promote adsorption of high metal ions (Conrad and Bruun Hansen 2007; Lee and Rowell 2004; Abad et al. 2002). Laboratory-scale column tests using cocopeat as an adsorbent with a bed volume of 110.0 cm<sup>3</sup> removed Pb, Cu, and Fe from an aqueous solution (Ong 2010), while Pb and Cd were sorbed at bed capacities of 41 mg/g and 28 mg/g of cocopeat, respectively (Amarasinghe

2011). Batch tests using cocopeat in an aqueous solution showed high removal efficiencies on Pb and Zn at pH 4.0 with an adsorbent dose of 1.0 g/L (Waskita et al. 2012); 91% at pH 4.5 for Zn and 97% at pH 2.5 for Pb with a dose of 20-22 g/L (Conrad and Bruun Hansen 2007); Pb at pH 4.0 with an adsorbent dose of 10 g/L (Hazeri et al. 2012). Co-copeat biomass has also been used in the adsorption of Pb, Cd, Cu ,and Ni ions in a multi-component aqueous solution (Vijayaraghavan et al. 2016), while Cu, Ni, and Zn were removed by pretreatment modified cocopeat using nitric acid (HNO<sub>3</sub>) and sodium hydroxide (NaOH) (Diola and Orozco 2014; Einollahipeer and Pakzadtoochaei 2013).

Although an extensive number of sorption studies have been conducted in synthetic waters with spiked heavy metal concentrations, sorbed onto various adsorbents including cocopeat, the conclusions obtained from these studies can only be applied to actual wastewaters to a very limited extent. Using actual wastewater samples in adsorption experiments is necessary if the objective of the experiment is to assess the potential of certain sorbents in actual wastewater treatment. In this study, cocopeat is used as an adsorbent to treat Hg and other heavy metals (As, Ba, Cd, and Pb) present in the wastewater of SSGM ball mill facility. The objective of this study is to gain an initial understanding on the adsorption mechanisms by conducting laboratory batch experiments using actual SSGM wastewater that would lead to the design and development of an on-site treatment facility.

# 2. MATERIALS AND METHODS

## 2.1 SSGM wastewater

Actual wastewater gathered from an SSGM ball mill facility in Paracale, Camarines Norte, Philippines, was used as samples in the study. Wastewater samples were collected from the outlet of a tailings collection tank inside the facility and brought to the laboratory for pH and total suspended solids (TSS) analyses. Total suspended solids were measured using the gravimetric method and dried at 105°C while pH was measured using a digital pH-EC-TDS meter (Hanna HI 98130, USA). Separate water samples were collected and placed in 1,000-mL polypropylene bottles and were put in a container with ice to preserve the samples during transportation from the site to the laboratory for heavy metal analyses. The physico-chemical characteristics of actual SSGM wastewater are presented in Table 1.

## 2.2 Plain settling

Wastewater was poured into a glass column (7.5 cm inside diameter and 120 cm high) for 60 min to reduce the suspended solids before analyzing its initial heavy metal concentrations. The optimum settling time was established

TABLE 1. Wastewater characteristics used in batch experiment.

Parameter	Unit	Actual SSGM wastewater	After 60 min settling	% reduction
рН	рН	6.88	7.30	-
TSS	g/L	0.87	0.235	27.01
As	mg/L	0.23	0.019	8.26
Ba	mg/L	0.02	0.02	0.00
Cd	mg/L	0.003	0.003	0.00
Hg	mg/L	0.0906	0.0035	3.86
Pb	mg/L	1.27	0.137	10.79

based on the results of a previous study that after 60 min of settling in the column, there were reductions of As (97.83%), Hg (95.14%), and Pb (93.70%) from the actual SSGM wastewater samples (Samaniego and Tanchuling 2018). After settling, water samples were analyzed for heavy metal and TSS concentrations to determine the reduction rate after 60 min. Settling resulted in a reduction of 27.01% on TSS, 8.26% on As, 10.79% on Pb, and 3.86% on Hg concentrations, while there were no concentration reductions observed on Ba and Cd (Table 1). Water samples collected from the settling column after 60 min were used samples for batch adsorption tests.

#### 2.3 Analytical methods

Heavy metal analyses used an Atomic Absorption Spectrophotometer (Agilent 55AA, USA) and followed the appropriate methods suggested in *Standard Methods for the Examination of Water and Wastewater* (Clescerl et al. 1998). Hydride generation AAS was used for As, flame AAS for Ba, Cd, and Pb, and cold vapor AAS for Hg. The limit of detection for the method used in analyzing the metals was 0.001 mg/L for As, 0.2 mg/L for Ba, 0.003 mg/L for Cd, 0.01 mg/L for Pb, and 0.0001 mg/L for Hg.

#### 2.4 Cocopeat batch adsorption tests

#### 2.4.1 Characterization and preparation of cocopeat

The cocopeat used as the adsorbent in this study was sourced from the stockpiles of Soriano Integrated Fiber Corporation coconut husk decorticating plant in Sariaya, Quezon Province. The same cocopeat was also used as the adsorbent in a number of previous studies on batch and column experiments to remove heavy metals from an aqueous solution (Ong 2010; Parcon 2010; Pingul 2010). Most of the physico-chemical characteristics of cocopeat assessed in the previous studies of Ong (2010), Parcon (2010), and Aquino et al. (2009) were also assessed in this study, in addition to several other important parameters such as bulk density, porosity, particle size and heavy metal contents unique to the present study.

Particle size distribution analysis was performed by following the procedures stated in ASTM D422-63. Cocopeat samples were sorted using Test Sieve No. 10 (W.S. Tyler, USA) to get a particle size of  $\leq 2$  mm and to eliminate long fibers and impurities. The sorted cocopeat was mixed to come up with a homogenous sample to be used in the

TABLE 2. Physical characteristics and heavy metal concentrations of the cocopeat used in the experiment.

Parameter	Value
Moisture Content (%)	38.28
Bulk Density, $\rho_b$ (g/cm <sup>3</sup> )	0.101
Particle Density (g/cm <sup>3</sup> )	1.56
Porosity, n (%)	93.46
Particle Size (mesh)	0.075–2 mm
Saturated hydraulic conductivity, K <sub>s</sub> (cm/hr)	70.04
Arsenic (mg/L)	N.D.
Barium (mg/L)	N.D.
Cadmium (mg/L)	N.D.
Mercury (mg/L)	0.208
Lead (mg/L)	N.D.

experiment and maintained its natural condition without washing or any chemical pre-treatment. The aforementioned technique was chosen to test the material under the simplest and most practical operational conditions, which may be adopted later on by the small scale gold mining processors. A summary of the physical characteristics and heavy metal concentrations of the cocopeat used in the experiment is presented in Table 2.

#### 2.4.2 Batch tests

Batch tests were carried out using the collected wastewater samples after 60 min of settling in a glass column. The measured pH of the entire wastewater samples was 7.30. Tests were conducted by mixing 100 mL wastewater with a 1.0 g/L adsorbent dose in a 250 mL Erlenmeyer flask. The flask with the solution was placed in an orbital shaker (Estuart SSL1 Orbital Platform Shaker, UK) set at a constant agitation speed of 200 rpm and withdrawn after the specified contact times of 10, 30, 60, 120, 180, 240, 360, and 540 min for As, Pb, and Hg, and 10, 30, 60, 120, 180, and 240 min for Cd and Ba. After mixing in an orbital shaker, the solution was filtered using Whatman #40 (USA) filter paper placed in a glass funnel. The Erlenmeyer flasks were washed with deionized water to remove cocopeat particles and heavy metal ions that may have been retained in the flask. Washed water was also filtered and mixed with filtrate. The collected filtrates were acidified by adding  $HNO_3$  until their pH reached <2. The samples were transferred into polyethylene sampling bottles and refrigerates and preserved for heavy metal analyses.

Adsorption of heavy metals using 0.10 g of cocopeat in 100 mL of wastewater was carried out in this study. Mixtures were agitated at 200 rpm in a shaker for 240 min, which was more than the ample time for adsorption equilibrium. The metal uptake  $q_t$  at time t was computed using Equation 1.

$$q_t = \frac{(C_i - C_t) V}{W} \tag{1}$$

where  $C_i$  is the initial metal concentration (mg/L),  $C_t$  is the metal concentration at time t (mg/L), V is the volume of metal solution used (L), W is the weight of adsorbent (g), and  $q_t$  is the amount of metal adsorbed at a given time t (mg heavy metal/g adsorbent).

### 2.4.3 Kinetic modelling

To identify the rate-controlling mechanisms during the adsorption of As, Ba, Cd, Hg and Pb, the following steps were considered, as described by Benavente et al. (2011); (1) mass transfer of the metal ions from the wastewater to the cocopeat surface, (2) adsorption of the metal ions onto sites, and (3) intra-particle diffusion of the metal ions onto cocopeat. For this purpose, simplified models were applied to evaluate the experimental batch data for each metal: a Lagergren first-order equation, a pseudo-second-order equation, and intra-particle diffusion.

The pseudo-first-order or Lagergren rate equation was the first rate equation for sorption in a liquid/solid system based on solid capacity, expressed with Equation 2

$$\frac{dq_t}{dt} = k_1 \left( q_e - q_t \right) \tag{2}$$

where  $q_e$  and  $q_t$  are the sorption capacities ( $\mu g/g$ ) at equilibrium and at time *t*, respectively, and  $k_1$  is a pseudo-first-

order sorption rate constant (1/min). By integration, assuming the boundary condition  $q_t = 0$  at t = 0 and  $q_t = q_t$  at t = t, the equation becomes that show in Equation 3.

$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303}t$$
(3)

where  $k_1$  (1/min) is calculated by plotting the function.

If the rate of adsorption has a second-order mechanism, the pseudo-second-order chemisorption kinetic rate equation is expressed by Equation 4 (Ho and Mckay 2000).

$$\frac{d_q}{d_t} = k_2 (q_e - q_t)^2 \tag{4}$$

where  $k_2$  is the pseudo-second-order sorption rate constant (g/(µg min)). Integration of Equation 4, assuming the boundary conditions  $q_t = 0$  at t = 0 and  $q_t = q_t$  at t = t, yields (Equation 5):

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t \tag{5}$$

where  $q_t$  is the amount of sorption ( $\mu g/g$ ) at time (min),  $q_e$  is the amount of sorption at equilibrium time ( $\mu g/g$ ), and  $k_2$  ( $g/(\mu g min)$ ) is calculated by plotting the function.

The intra-particle diffusion model in this study was explored using the Weber-Morris equation (Equation 6), as described by Kaczala et al. (2009).

$$q_t = k_i t^{\frac{1}{2}} + c \tag{6}$$

where  $q_t$  is the amount adsorbed at time t (µg/g), t is the contact time (min),  $k_i$  is the intra-particle diffusion rate constant (µg/(g min<sup>1/2</sup>)), and  $k_i$  and c are calculated by plotting the function.

#### 2.4.4 Freundlich isotherm equation

The Freundlich equation is an empirical relationship describing the adsorption of solutes from a liquid to a solid surface. It gives an expression encompassing the surface heterogeneity and the exponential distribution of active sites and their energies (Abdel Salam et al. 2011). The Freundlich model was applied since this model is considered suitable, particularly for low to intermediate concentration ranges (Kaczala et al. 2009). The general form of this model is (Equation 7):

$$q_e = K_F C_e^{\frac{1}{n}} \tag{7}$$

Equation 7 can be linearized by taking the logarithm of both sides of the equation and will result in Equation 8.

$$\log q_e = \log K_F + \frac{1}{n} \log C_e \tag{8}$$

where  $C_e$  is the equilibrium concentration ( $\mu g/g$ ),  $q_e$  is the adsorbed amount at equilibrium ( $\mu g/g$ ), and  $K_F$  and  $\frac{1}{n}$  are the Freundlich constants.  $K_F$  and  $\frac{1}{n}$  are experimentally calculated by plotting the function.

#### 3. RESULTS AND DISCUSSION

The present study did not analyze the effect of pH on adsorption efficiency because its objective was to apply a filter bed adsorption system using cocopeat to the SSGM ball mill facility without any adjustment in pH and other physicochemical properties of the wastewater. Furthermore, only an adsorbent dose of 1.0 g cocopeat/L was used in the experiment because applying a higher dosage resulted in adsorption of more ions or complete sorption of ions from the sorbate. The room temperature during batch tests ranged from 25 to 27°C.

## 3.1 pH development during adsorption

During the batch adsorption test, pH development was monitored with respect to contact time. With an initial pH of 7.30, it decreased to pH 7.15 in the first 10 min but then went up to pH 7.79 after 240 min of contact time (Figure 1). The initial decrease of pH observed conforms with the study conducted by Kaczala et al. (2009) on the adsorption of Pb onto sawdust. Such an increase of hydrogen ions might be related to deprotonation of acidic groups present in lignin, as pointed out by Ho and Mckay (2000) during the sorption of Pb onto lignin-based fern tree adsorbent. Such observations were also observed in the present study.

## 3.2 Removal efficiency

The removal efficiency obtained for the heavy metals with the initial pH of 7.30 at a 1.0 g/L adsorbent dose after 240 min is shown in Figure 2. The highest removal efficiency was achieved by Hg (97.14%), followed by As (94.74%), Cd (66.67%), Pb (27.01%), and Ba (10.00%). High removal efficiencies can be attributed to low initial concentrations of heavy metal adsorbed, as demonstrated in the efficiency of Hg and its low initial concentration, while a low removal efficiency was found with Pb, which had a high initial concentration. As presented in Figure 2, the order from the highest removal efficiency (Hg>As>Cd>Pb>Ba) is inversely related to the sequence from highest to lowest initial concentrations of wastewater used in the experiment (Pb>Ba>As>Cd>Hg). The varied range of initial concentra-



FIGURE 1. pH development over time during batch tests using 1.0 g cocopeat/L.



FIGURE 2. Removal efficiency (%) and initial concentration for heavy metals at t = 240 min with 1.0 g/L adsorbent dose.

tions of different heavy metals present in the actual SSGM wastewater is traced from the composition of mined ores while Hg concentration in wastewater was directly related to the use of Hg in amalgamation. The longer time required to attain the equilibrium (240 min) in this study is probably related to the complexity of the actual wastewater tested, where different organic and inorganic compounds compete for sorptive sites, compared with the spiked synthetic water used in previous studies with cocopeat (Waskita et al. 2012; Conrad and Bruun Hansen 2007; Hazeri et al. 2012).

### 3.3 Effect of contact time

Effect of contact time on As, Ba, Cd, Hg, and Pb uptake rate by cocopeat with an initial pH of 7.30 are shown in Figures 3a-e. At an adsorbent dose of 1.0 g cocopeat/L, the concentrations on solid phase were increased until reaching their respective equilibrium concentrations. The solid phase concentrations for As, Ba, Cd, and Hg were erratic in the first 120 min, but at 180 min, the cocopeat adsorption reached its equilibrium. At the first 120 min, the liquid phase concentration of Pb increased (Figure 3e), resulting in a higher negative reduction for the solid phase. At 180 min, the solid phase concentration for Pb on cocopeat increased, but it was still low at the end of 240 min, and by prolonging the contact time, there were no more changes observed in the adsorption.

In this study, longer contact time (from 240 to 540 min) for As, Hg, and Pb to attain equilibrium was probably related to the complexity of the mining wastewater tested, where different organic and inorganic compounds compete for sorptive sites (Kaczala et al. 2009), compared with the heavy metal-spiked distilled water used in previous studies with cocopeat (Ong 2010; Parcon 2010; Pingul 2010; Waskita et al. 2012).

# 3.4 Kinetic modelling

#### 3.4.1 Lagergren first-order model

The resulting parameters from the linearized adsorption data of the kinetic batch experiment to Lagergren firstorder model for As, Ba, Cd, Hg, and Pb with an initial pH

TABLE 3. Lagergren first-order parameters for heavy metals adsorption onto cocopeat.

Adsorbent (1.0 g/L)	k <sub>1</sub> (1/min)	q <sub>exp</sub> (µg/g)	q <sub>calc</sub> (µg/g)	Deviation (%)	R <sup>2</sup>
As	0.0041	18.00	5.45	69.72	0.6525
Ba	0.0016	2.00	1.34	33.00	0.2753
Cd	0.0032	2.00	1.58	21.00	0.3019
Hg	0.0039	3.41	0.23	93.25	0.0729
Pb	0.0053	57.00	45.39	20.37	0.2049

TABLE 4. Pseudo second-order parameters for heavy metal adsorption onto cocopeat.

Adsorbent (1.0 g/L)	k1 (g/(µg min))	q <sub>exp</sub> (µg/g)	q <sub>calc</sub> (µg/g)	Deviation (%)	R <sup>2</sup>
As	0.0023	18.00	18.98	5.16	0.9924
Ва	0.0125	2.00	2.13	6.10	0.7463
Cd	-0.0502	2.00	1.83	8.50	0.9559
Hg	1.3551	3.41	3.66	6.83	0.9410
Pb	-0.0000155	57.00	6.05	89.38	0.7358



FIGURE 3. Effect of contact time on As (a), Ba (b), Cd (c), Hg (d), and Pb (e) uptake rate by cocopeat with initial pH of 7.30 and adsorbent dose of 1.0 g/L.

of 7.30 at an adsorbent dose of 1.0 g/L are presented in Table 3. All heavy metals tested did not fit well with low computed linear regression correlations  $R^2$  ranging from 0.0729 to 0.6525. This suggests that the first-order model cannot be considered as the sorption process of heavy metals onto cocopeat.

### 3.4.2 Pseudo-second order model

The results of pseudo-second order adsorption for the heavy metals onto cocopeat are shown in Table 4. The correlation coefficients for the second-order kinetics model ( $R^2$ ) are higher compared with those of the first-order equation, indicating the applicability of this kinetic equation and the second-order nature of the adsorption process of heavy metals onto cocopeat. In addition to the high  $R^2$  values, the theoretical and experimental values of  $q_e$  obtained low percentages of deviation, suggesting that pseudo-second-order kinetics can be considered as the sorption process of heavy metals onto cocopeat.

In the case of Pb, the  $q_{exp}$  (57.00 µg/g) is high compared with the  $q_{calc}$  (6.05 µg/g), which is due to the complexity of the actual wastewater used in the experiment, as shown in Figure 3e. Although it presents a very high deviation, it can still be considered and fitted to the pseudo second-order model as it has a higher R<sup>2</sup> value than the first-order model. Negative (-)  $k_2$  values for Cd (-0.0502 g/(µg min)) and Pb (-0.0000155 g/(µg min)) are attributed to the rapid uptake followed by desorption in the first 120 min, as illustrated in Figure 3e. The pseudo-second order model can be considered a kinetics model based on the assumption that the rate limiting step may be a chemical adsorption (chemisorption) as it provides a correlation of the data.

## 3.4.3 Intra-particle diffusion model

The linearity of the curve for the intra-particle diffusion model had a wide range of  $\mathbb{R}^2$ , between 0.0454 and 0.8394 (Table 5). These indicate that the linearity may not be the basis for the selection of the rate limiting step of heavy metal adsorption onto cocopeat. The rate constants ( $k_i$ ) characteristic of the adsorption in the region where intraparticle diffusion is rate controlling. Based on the linear plots from the origin (*y*-intercept other than 0) indicates that there are other sorption steps such as external diffusion (Kaczala et al. 2009).

In summary, among the three kinetic models evaluated in this study, the pseudo-second order kinetics model represented well the adsorption process, as demonstrated with its higher correlation coefficients,  $R^2$  values in all heavy metals compared with the pseudo-first order and intra-particle diffusion models. The applicability of pseudo-second order kinetics suggests that the rate limiting step may be a chemical adsorption or chemisorption as the sorption process of heavy metals onto cocopeat. This result is in accordance with the sorption process of heavy

TABLE 5. Kinetic parameters of heavy metal intra-particle diffusion onto cocopeat.

Adsorbent (1.0 g/L)	k <sub>i</sub> (g/(µg min <sup>1/2</sup> ))	c (Intercept)	R <sup>2</sup>
As	0.4234	9.664	0.7654
Ва	0.1453	-0.1953	0.8394
Cd	0.1724	-0.3664	0.6872
Hg	0.0321	2.7217	0.0726
Pb	2.7509	-12.515	0.0454



FIGURE 4. Sorbate concentration after batch test using 2.5 g cocopeat/L (a) and 5.0 g cocopeat/L (b).

metals onto cocopeat using synthetic water in the studies of Ong (2010) and Waskita et al. (2012).

## 3.5 Adsorption isotherm

The batch experiment performed in this study used an adsorbent dose of 1.0 g cocopeat/L of sorbate at an initial pH of 7.30 and temperature range of 25–27°C. In an attempt to determine the Freundlich constants, additional batch tests using higher adsorbent doses (2.5 g cocopeat/L and 5.0 g cocopeat/L) were performed to determine the  $K_F$  and 1/n of each heavy metal. After the batch tests, the results showed that all of the heavy metals except for Hg had concentrations that were below the detection limits of the AAS used for the heavy metal analyses, as shown in Figures 4a-b. The increase in Hg concentration in the effluent after 180 min (2.5 g cocopeat/L) and 120 min (5.0 g cocopeat/L) was caused by the desorption of Hg ions present in the cocopeat, and which had an initial concentration of 0.208 mg/kg.

Considering the results of the batch tests with high adsorbent doses, the calculation of  $K_F$  and 1/n constants from the adsorption equilibrium of As, Ba, Cd, and Pb becomes impossible due to the absence of the trend in the results, thus no  $q_e$  and  $C_e$  were accepted. In the case of Hg, the increase in the sorbate concentration after 120 min caused by desorption may cause an unfavorable sorption intensity if used to calculate the  $K_F$  and 1/n constants.

# 4. CONCLUSIONS

In the present study, wastewater collected from the ball mill facility of a small scale gold mining site is characterized with a high concentration of Hg and other heavy metals, as well as suspended solids. Untreated cocopeat was used as an adsorbent in batch tests and demonstrated a capability to reduce heavy metals from actual SSGM wastewater that is complex in nature. Batch adsorption experiments were carried out using actual wastewater samples with reduced suspended solids collected after 60 min of settling and without modifying the pH (pH 7.30) and other parameters to simulate the actual conditions in the field. The settling process prior to sorption was proven to be an important step concerning the treatment of wastewater containing heavy metals.

After an equilibrium time of 240 min, batch tests with an adsorbent dose of 1.0 g cocopeat/L resulted in high removal efficiencies for Hg (97.14%), followed by As (94.74%), Cd (66.67%), Pb (27.01%), and Ba (10.00%). High removal efficiencies can be attributed to low initial concentrations of heavy metals adsorbed, as demonstrated in the efficiency of Hg and its low initial concentration. This is probably related to the complexity of the actual wastewater tested, where different organic and inorganic compounds compete for sorptive sites, compared with the spiked synthetic water used in previous studies with cocopeat.

Among the three kinetic models evaluated in this study, the pseudo-second order kinetics model best represented the adsorption process, as shown in its higher correlation coefficients ( $R^2$ ). The applicability of pseudo-second-order kinetics suggests that the rate limiting step may be a chemical adsorption or chemisorption as the sorption process of heavy metals onto cocopeat.

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